

## Sprayable Hotmelt Adhesive

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ins B2

This invention relates to a sprayable hotmelt adhesive based on a substantially amorphous poly- $\alpha$ -olefin (APAO) with a softening point (ring-and-ball method) of 70 to 130°C, a melt viscosity at 190°C of 1,000 to 20,000 mPas and an addition of resins and oils. The present invention also  
5 relates to the production of this hotmelt adhesive and to its use.

ins B3

A sprayable hotmelt adhesive is already known. Thus, EP 0 442 045 B1 describes a sprayable hotmelt adhesive based on the above-mentioned poly- $\alpha$ -olefin with no more than 30% by weight of additives, more especially waxes and/or resins. Paraffinic or aromatic oils may also  
10 be used. The Examples contain ethene/propene/1-butene terpolymers and plastic microwaxes and, in some cases, even a hydrocarbon resin. The viscosities are in the range from 2,700 to 3,400 mPas at 190°C.

The Hüls technical information pamphlet entitled "Vestoplast: Klebrohstoff für Hot-Melt-Anwendungen (Vestoplast: an Adhesive Raw  
15 Material for Hotmelt Applications)" dating back to 1996 describes a number of atactic poly- $\alpha$ -olefin copolymers and terpolymers of the monomers ethylene; propylene and 1-butene. Polymers such these have excellent wetting behaviour on nonpolar substrates such as, for example, polyethylene and polypropylene. An increase in adhesive strength can be  
20 achieved by combination with tackifying resins or plasticizers. Recommended resins include, in particular, substantially saturated hydrocarbon resins. Added in a quantity of up to 30%, the resin acts as a plasticizer. Beyond 35%, the mixture assumes the properties of the resin and becomes hard and brittle. The tensile strength of a mixture of poly- $\alpha$ -  
25 olefin and resin in a ratio of 70:30 parts by weight falls by at least 20% when the ratio is changed to 50:50 parts by weight at the expense of the poly- $\alpha$ -olefin. Waxes are added inter alia for fine viscosity adjustment and

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to reduce stringing. In most cases, polybutenes of relatively low molecular weight are recommended as plasticizers. It costs less to use paraffinic or naphthenic mineral oils. The basic formulation for sprayable hotmelt adhesives for sanitary articles contains 70 parts of Vestoplast 704 (a poly- $\alpha$ -olefin), 25 parts of Escorez 5380 (a hydrogenated polycyclopentadiene), 5 parts of Napvis D 10 (a polybutene liquid at room temperature) and 0.4 part of Irganox 1010 (an antioxidant for polyolefins). This known sprayable hotmelt adhesive has a melt viscosity of 2,000 mPas at 190°C and a softening point of 91°C. Unfortunately, it has poor adhesive properties.

Thus, the initial adhesion values in particular are poor and deteriorate even further in the event of storage. Further disadvantages include a distinct reduction in the adhesion values in the wet state, the so-called "wet values" or "wet strength". Since the adhesives described in the document in question are used in particular for the production of a composite material, for example for a composite material containing at least one nonwoven, it is essential that the adhesion values after storage and the wet adhesion values do not fall below the initial values. The adhesives are being used to an increasing extent in many areas of everyday life because, in general, they represent a simple, permanent and safe method of fixing materials.

Composite materials of the type used in particular in the field of personal hygiene are generally materials with a limited useful life which are discarded, for example, after being used only once, more especially disposable products. Products such as these mainly include diapers, sanitary towels and panty liners etc. of which the function is to absorb bodily fluids such as, for example, urine and blood. In view of this fact, the adhesive used in the composite material must hold the material together even in the "wet" state. This is only possible if the so-called wet values are at the same level as the initial values.

EP 211 311 describes a self-adhesive absorbent shaped body and a process for the production of a pressure-sensitive hotmelt adhesive

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5 suitable therefor. The pressure-sensitive hotmelt adhesive consists of 20 to 80% of substantially amorphous olefinic polymers, 20 to 80% of tackifying resins and 0 to 80% of plasticizer oil, the polymers being atactic and the pressure-sensitive hotmelt adhesive having a shear strength of less than 1 minutes (standard test against steel). Only one olefinic polymer is mentioned. It has a melt viscosity at 190°C of ca. 50,000 mPas.

10 Accordingly, the problem addressed by the present invention was to improve adhesion, above all initial adhesion, but also adhesion after storage for a certain period and also wet adhesion. In addition, however, the adhesion levels would be made more independent of the processing conditions, more especially the spraying temperature, the quantity applied and the method of application. However, the spraying properties and other important processing and performance properties would not be adversely affected.

15 *ans BY* The solution provided by the invention is defined in the claims and consists essentially in the composition of the sprayable hotmelt adhesive, namely

- 20 A) 30 to 70% by weight and preferably 35 to 50% by weight of at least one substantially amorphous poly- $\alpha$ -olefin or poly- $\alpha$ -olefin mixture with a softening point (ring-and-ball method) of 70 to 130°C, a melt viscosity at 190°C of 1,000 to 20,000 mPas and preferably with a density of <0.90 g/cm<sup>3</sup>, a needle penetration of 8 to 4.0 mm, a molecular weight as determined by gel permeation chromatography of at most 100,000 (weight average) or at least 4,000 (number average), the difference
- 25 between the weight average and the number average molecular weight being no more than six times the number average,
- 30 B) 5 to 30% by weight and more particularly 15 to 25% by weight of at least one oil of a saturated hydrocarbon of relatively low vapor pressure which is liquid at 20°C, more especially at least one mineral oil with a paraffinic or naphthenic base and, above all, at least one medicinal

white oil,

- 5 C) 20 to 60% by weight and more particularly 25 to 50% by weight of at least one hydrocarbon resin with a softening range of 70 to 140°C and, more particularly, 80 to 120°C, suitable hydrocarbon resins being above all resins containing 5 to 9 carbon atoms and including partly or completely hydrogenated, aliphatic and aromatic hydrocarbon resins, polyterpene resins and modified polyterpene resins and also natural resins, and
- 10 D) optionally additives, such as heat and light stabilizers, optical brighteners, antistatic agents, lubricants and antiblocking agents, nucleating agents, dyes, pigments and flame retardants,

with a viscosity of 500 to 4,000 mPas and, more particularly, in the range from 700 to 1,900 mPas, as measured in accordance with ASTM D 3236-88 (Brookfield Model RVT DV II, 150°C, spindle 27).

15 *en 585* The poly- $\alpha$ -olefins (component A) are polymers of the type described in EP 0 442 045 B1 of which the disclosure is hereby specifically included as part of the present application.

Preferred polyolefins are either completely amorphous or have only  
20 minimal crystallinity. Accordingly, the heat of fusion for heating to 180°C ( $\Delta H$ ) by DTA analysis in accordance with DIN 53765 should only be between 330 and 500 J/g and, more particularly, between 370 and 450 J/g while the specific heat capacity from 20 to 200°C by DTA analysis in accordance with DIN 53765 should be between 1.0 and 4.0 J/g·K and, more  
25 particularly, between 1.7 and 3.2 J/g·K. The glass transition temperature  $T_g$ , which is also to be determined by DTA analysis in accordance with DIN 53765, should be in the range from -15°C to -40°C and, more particularly, in the range from -20°C to -38°C. Suitable products may be produced, for example, by radical degradation of commercially available substantially  
30 amorphous poly- $\alpha$ -olefins with softening points of 80 to 140°C and

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viscosities of 5,000 to 100,000 mPas at 190°C. This method of production is the subject of German patent application P 40 00 695.6. However, they may also be produced by any other process providing they then have the claimed features.

5            Suitable substantially amorphous poly- $\alpha$ -olefins may carry functional groups to improve adhesion to standard substrates. These functional groups may be introduced either by copolymerization with small quantities of functional monomers or, preferably, by radical reaction of commercially available poly- $\alpha$ -olefins with such functional monomers. Suitable mono-  
10        mers are, for example, maleic anhydride, fumaric acid, acrylic and methacrylic acid, itaconic acid, aconitic acid and derivatives thereof such as, for example, esters or amides and vinyl trimethoxysilane (VTMO) and 3-methacryloxypropyl trimethoxysilane (MEMO;  $\text{H}_2\text{C} = \text{C}(\text{CH}_3)\text{COO}(\text{CH}_2)_3\text{Si}(\text{OCH}_3)_3$ ). They are normally used in quantities of 0.1 to 10% by weight  
15        and preferably in quantities of 0.5 to 5% by weight, based on the poly- $\alpha$ -olefin. Standard radical initiators such as, for example, dicumyl peroxide or 2,2'-azo-bis-(2-acetoxypropane) are used in quantities of 0.05 to 3% by weight and preferably 0.1 to 2% by weight. The grafting reaction then takes place at elevated temperatures, generally in the range from 100 to  
20        300°C. Polymers with high cohesion and improved adhesion to certain substrates, such as metal, plastic or glass surfaces, are obtained in this way.

*Sub 17*

~~In one preferred embodiment, the substantially amorphous poly- $\alpha$ -olefin is a binary or ternary copolymer of olefins containing 2 to 10 carbon atoms. This copolymer preferably has the following monomer composition: 3 to 75% by weight of an  $\alpha$ -olefin containing 3 to 10 carbon atoms, 25 to 95% by weight of propene and 0 to 20% by weight of ethene.~~

In addition, the copolymer may also contain functional monomers, as  
30        already mentioned. In one particularly preferred embodiment, 1-butene is

used as the  $\alpha$ -olefin containing 4 to 10 carbon atoms. Mixtures of different poly- $\alpha$ -olefins according to the invention may of course also be used.

5 ~~sub B~~ The poly- $\alpha$ -olefin mixture preferably contains at least one poly- $\alpha$ -olefin with a melt viscosity of 40,000 to 60,000 and at least one poly- $\alpha$ -olefin with a melt viscosity of 3,000 to 10,000 Pas at 190°C.

The melt viscosity of the poly- $\alpha$ -olefin or the poly- $\alpha$ -olefin mixture is advantageously in the range from 2,000 to 15,000 mPas at 190°C.

Poly- $\alpha$ -olefins such as these are commercially available under such names as Vestoplast®, Rexene®, etc.

10 Component B comprises oils of substantially saturated hydrocarbons of relatively low vapor pressure which are liquid and, in particular, thinly liquid (20 to 300 mPas) at 20°C, more especially mineral oils with either a paraffinic base or a naphthenic base and, above all, medicinal white oils which are approved for use in foods under FDA 175 105. These white oils  
15 have a viscosity of 25 to 230 mPas and, more particularly, in the range from 110 to 230 mPas, as measured in accordance with DIN 51562 at 20°C. These oils are used inter alia for fine viscosity adjustment. They are commercially available under such names as Primol352®, Essomarc® oils, Pionier 0352®, Drakeol 35®, Kaydol®, Ondina G® oils, Catenex N®  
20 oils, etc.

Component C contains above all a hydrocarbon resin of C<sub>5-9</sub> structural units, more particularly a substantially and, more particularly, completely hydrogenated polycyclopentadiene resin as the hydrocarbon resin. Specific examples are MBG® resins, Regalite R and S® resins,  
25 Zonarez® resins, Zonatac® resins, Betaprene® AC, AF, AK, AR, B, BC, BR resins, Betalite® resins, Eastotac® resins, ECR® resins, Escorez® resins, Wingtack® resins, etc.

Components B and C together should make up at least 30% by weight, preferably at least 35% by weight and more preferably at least 45%  
30 by weight, based on the sum of components A, B and C. In other words,

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the poly- $\alpha$ -olefin content should be at most 70%, more particularly at most 65% and above all at most 55% by weight, based on components A, B and C.

In order to obtain a particularly uniform spray pattern, even at relatively low melting temperatures of, for example, 130°C, components A, B and C should be selected within the claimed range so that the melt viscosity at 100°C is in the range from 5 to 15 Pas  $\pm$  15, more particularly  $\pm$  10%, depending on the shear rate between 0 and 250 sec<sup>-1</sup>. Even at 130°C, it shows non-newtonian flow behaviour. The measurements were carried out to DIN 53018-1.

The hotmelt adhesives according to the invention are preferably non-pressure-sensitive hotmelt adhesives. Besides the percentage contents of components A, B and C, the choice of the nature of the components is very important. Thus, the melt viscosity of the poly- $\alpha$ -olefin or the poly- $\alpha$ -olefin mixture should be between 2 and 15 Pas at 190°C (Brookfield).

Besides these essential components, other substances, for example heat and light stabilizers, optical brighteners, antistatic agents, lubricants and antiblocking agents, nucleating agents and dyes, pigments and flame retardants, may also be added.

A suitable antioxidant is, above all, Irganox 1010 used in a quantity of 0 to 3% by weight, based on the hotmelt adhesive as a whole. Other suitable stabilizers are, above all, Irganox PS 800, Irgastab DBTM, Tinuvin P, Wingstay stabilizers, Wingstay SN-1, Evernox 10, etc.

Fully synthetic thermoplastic polymers, especially polypropylene, may also be added, for example to modify the softening temperature. Suitable polypropylene types include atactic polypropylene, homopolypropylene, statistical copolymers, block copolymers and graft copolymers of propylene. However, other synthetic polymers may also be used, including for example ethylene/vinyl acetate copolymers, ethylene/acrylic acid

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copolymers, polyisobutene, polybutene, isotactic poly-1-butene, styrene block copolymers and rubber. They make up from 0 to 50% by weight and preferably from 15 to 45% by weight of the hotmelt adhesive as a whole.

To produce the hotmelt adhesive, the raw materials mentioned  
5 above are mixed in the melt in an inert gas atmosphere and/or in a vacuum until they are homogeneous. The temperature of the melt is preferably from 150 to 200°C. It is important to ensure that there are no specks in the hotmelt adhesive produced.

The hotmelt adhesive obtained is largely characterized by its  
10 viscosity of 500 to 4,000 mPas and preferably 700 to 1,900 mPas at 150°C, as measured to ASTM D 3236-88 (Brookfield Model RVT DVII; 150°C; spindle 27). It is also characterized by its favorable sprayability both in regard to "atomization" of the melt and in regard to so-called "spin spraying". In the first of these two processes, the melt is atomized into fine  
15 melt droplets whereas, in "spin spraying", a melt strand leaves the spray nozzle in a spiral and, without breaking, is deposited in a spiral pattern onto the substrate to the coated. This spraying technology generally allows contactless application and the coating of uneven irregular surfaces. It is also suitable for applications where, although bonding over a certain area  
20 may be required, the bonded area must be permeable to air or moisture. The fact that the adhesive is not applied over the entire area means that material can be saved.

Another advantage arises in the coating of heat-sensitive substrates. By virtue of the contactless application and the very low heat content of the  
25 melt or melt strand applied, the substrate undergoes less stressing or damage than is the case in conventional methods of application. Hotmelt spraying technology is environmentally friendly and, overall, covers many applications which, hitherto, have been the preserve of sprayed solvent-based adhesives.

30 The favourable sprayability naturally applies both to the

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"atomization" mentioned earlier on and to "spin spraying". A uniform spray pattern produced by spin spraying requires a viscosity of the adhesive to be sprayed which is largely independent of the shear rate at the particular application temperature. If this were not the case, it would not be possible to achieve a constant spraying width, for example in intermittent spraying. Both at the beginning and at the end of the particular spraying cycle, the viscosity would be increased on account of the lower shear rate so that the spray pattern would change.

The spraying behavior is distinguished in particular by the following properties:

- a) Temperature variations between 140 and 160°C affect the adhesion values to an extent of only  $\pm 14\%$ , based on a coating weight of 4 g/m<sup>2</sup>.
- b) Variations in the coating weight of 2 to 4 g/m<sup>2</sup> affect the adhesion values to an extent of only  $\pm 7\%$ .
- c) Such methods of application as "Control Coat" or spin spraying also have only a slight effect (namely  $\pm 6\%$ ) on the adhesion values.

Other positive properties of the hotmelt adhesive according to the invention include not only its high early adhesion, but also the increase in the adhesion values after ageing. They are in the range from 20 to 60%. Other positive properties of the adhesives according to the invention include the increase in wet strength by 29% to 126% and fiber failure of the composite material after ageing both in regard to wet strength and in regard to early adhesion.

The hotmelt adhesives according to the invention are suitable for bonding various materials. Thus, such materials as polyolefin films, for example polyethylene films or polypropylene films, polyolefin nonwovens, for example polyethylene nonwovens or polypropylene nonwovens, polyurethane films, polyurethane foams, films or mouldings of cellulose

derivatives, for example tissues, films or moldings of polyacrylates or polymethacrylates, films or mouldings of polyesters, can be bonded to one another. The hotmelt adhesives according to the invention may be used to bond materials of the same kind and materials of different kinds to one another.

In one preferred embodiment of the process according to the invention, the adhesive is used in the production of a composite material containing at least one nonwoven layer. In a particularly preferred embodiment, the nonwoven layer is a polypropylene spunbonded with a weight per unit area of about 10 to about 30 g/m<sup>2</sup> and, more particularly, about 15 to about 20 g/m<sup>2</sup>.

A nonwoven layer, preferably one containing or consisting of a polyolefin, is particularly suitable as the second material to be bonded to the substrate.

In the context of the present invention, a "nonwoven layer" is understood to be a flexible material which is not produced by conventional warp/weft weaving or by loop formation, but rather by the interlocking and/or cohesive and/or adhesive bonding of textile fibers. Accordingly, nonwovens are understood to be loose materials of spun fibers or filaments, generally of polypropylene, polyester or viscose, which are generally held together by the adhesion inherent in the fibers. The individual fibers may have a preferential orientation (oriented or cross-laid nonwovens) or no orientation (random laid nonwovens). The nonwovens may be mechanically strengthened by needle punching, stitching or lacing by sharp jets of water (so-called spunlaced nonwovens). Adhesively strengthened nonwovens are formed by bonding the fibers with liquid binders (for example acrylate polymers, SBR/NBR, polyvinyl ester or polyurethane dispersions) or by melting or dissolving so-called binding fibers which have been added to the nonwoven during its production. In the case of cohesive strengthening, the fiber surfaces are dissolved by

suitable chemicals and joined by pressure or welded at elevated temperature. Nonwovens of so-called spunbondeds, i.e. materials produced by spinning and subsequent deposition, blowing or floating on a conveyor belt, are known as spunbonded nonwovens. Nonwovens  
5 containing additional filaments, woven or knitted fabrics count as reinforced or strengthened nonwovens.

In one preferred embodiment of the process according to the invention, the adhesive is used for the production of a composite material containing at least one nonwoven layer, above all for bonding films, more  
10 particularly of polyolefins, and nonwovens, more particularly of polypropylene, the application temperature being between 120 and 180°C and preferably between 140 and 160°C, the coating weight varying between 2 and 10 and preferably between 3 and 4 g/m<sup>2</sup> and the application rate preferably being between 50 and 400 m/min. In a particularly  
15 preferred embodiment, the nonwoven layer is a polypropylene spunbonded with a weight per unit area of about 10 to about 30 g/m<sup>2</sup> and, more particularly, in the range from about 15 to about 20 g/m<sup>2</sup>.

By virtue of these positive properties, the hotmelt adhesives according to the invention are suitable for structural bonding in sanitary  
20 products, more especially for bonding diapers and sanitary napkins.

Further applications are in the packaging industry, the automotive supply industry, the building industry, etc.

The invention is illustrated by the following Examples.

25 **I Starting materials for the production of the hotmelt adhesives**

1. Poly- $\alpha$ -olefins: Vestoplast 508, 704 and 750 (terpolymers of ethylene, propylene and butylene) of Hüls AG
2. Oils: Primol 352, a medicinal white oil manufactured by Esso
3. Resins: MGB-278 and Regalite R-R91 (cyclopentadiene resins) of  
30 Hercules

4. Antioxidants: Irganox 1010 of Ciba Geigy.

## II Production and properties of the hotmelt adhesives

5 To produce the hotmelt adhesives, the starting materials mentioned above are melted at 160 to 170°C in the quantities shown in Table 1a) in the following order: oil + antioxidant, resin and poly- $\alpha$ -olefin, and stirred at 160 to 170°C until the mixture is speck-free (homogeneous). This generally takes 2 to 4 hours. It is also advisable to apply a vacuum and/or an inert gas atmosphere (nitrogen).

10 The hotmelt adhesives obtained have the properties set out in Table 1b).

## III Adhesive testing of the hotmelt adhesives

1. The spraying tests were carried out with a Meltex CT 325 sprayer  
15 (manufacturer: Meltex, Lüneburg). The spray heads used were Nordson models CF 203 and CF 205 (the abbreviation CF stands for controlled fiberization). In the CF spray heads used here, a spiral movement is imparted to the adhesive issuing from the nozzle by compressed air. This procedure provides for the controlled, surface-covering and edge-sharp  
20 application of hotmelt adhesives.

	Quantity applied:	3.0 to 4.0 g · m <sup>-2</sup>
	Application rate:	100 m · min. <sup>-1</sup>
	Temperature in the melting tank:	160°C
25	Temperature of the spraying air:	180°C
	Adhesive temperature:	160°C.

Composite materials were produced on the basis of these parameters. On the one hand, the adhesive was sprayed onto the film  
30 while the nonwoven moved in the opposite direction; on the other hand, the

adhesive was sprayed onto the nonwoven while the film moved in the opposite direction. In addition to these tests carried out at an adhesive temperature of 160°C (tests A), tests were also carried out at an adhesive temperature of 140°C (tests B).

5           The film used was a 4P PE film, i.e. a polyethylene film with a thickness of about 10 to about 50 µm and, more particularly, about 20 to about 30 µm. The nonwoven used was Corosoft Plus H, a nonwoven of polypropylene with a weight per unit area of 14 to 30 g/m<sup>2</sup> and, more particularly, 17 g · m<sup>-2</sup>. In case a), the hotmelt adhesive was sprayed onto  
10       the film which was then bonded to the nonwoven. In case b), the adhesive was sprayed onto the nonwoven which was then bonded to the film.

2.       The adhesion value tests are summarized in Table 1c).

#### 15   IV Results

By comparison with the reference product, the tests of Examples 1 and 2 show

- a distinct increase in early strength up to fiber failure irrespective of the coating weight and irrespective of the production of the composite (in  
20       other words, there was a distinct improvement in the adhesion values in the film/nonwoven composite and in the nonwoven/film composite),
- a distinct increase in the adhesion values with fiber failure after ageing, based on the early strength, irrespective of the production of the composite and
- 25       • a distinct increase in the wet adhesion values with fiber failure, based on the early strength, irrespective of the production of the composite and
- a distinct step-by-step reduction in the adhesion values of the reference product after ageing and in the wet test.

**V Description of the test methods:**

- Melt viscosity to ASTM D 3236-88, Brookfield Model RVT DV II, 150°C, spindle 27,
- softening point to ASTM E 28,
- 5 • needle penetration (100/25/5) to DIN 52010 in 0.1 mm,
- peel strength (so-called adhesion value) to DIN 53530 using a Zwick 1435 tensile tester at 20°C/50% relative air humidity. The 50 mm wide sample is separated at a rate of 300 mm/min. at an angle of 180°. The result is expressed in  $\text{Ncm}^{-1}$ . The coating of the sample was measured
- 10 at the earliest after 48 h.
- Ageing behavior was simulated by so-called accelerated ageing (72 h at 60°C with a subsequent cooling time of at least 24 h).
- Wet strength (the sample to be tested is placed for 1 h in a 0.9% sodium chloride solution and then tested, internal test).
- 15 • Crystallinity by DTA analysis to DIN 53765.
- Density to DIN 53479
- Flow behavior to DIN 53018-1.

The rheological tests of the hotmelts were carried out with a TA  
20 Instruments AR 1000 rotational viscosimeter. To this end, a plate/plate geometry (4 cm diameter, 500  $\mu$  interval) was used in the shear-rate-dependent flow test. The adhesive was heated for 5 minutes at the measuring temperature between the plate/plate geometry. The viscosity was then measured continuously for 5 minutes as a function of the shear  
25 rate of 0 to 250  $\text{s}^{-1}$  or 250 to 0  $\text{s}^{-1}$ . In the case of samples with newtonian flow behaviour, viscosity is independent of the shear rate.

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Table 1a):

Composition of the hotmelt adhesives

Raw materials			Hotmelt adhesive		
Type	Commercial name/percentage		Example 1	Example 2	Comparison
APAO	Vestoplast 704	%	22.5%	35.0%	70%
APAO	Vestoplast 508	%	22.5%	-	-
APAO	Vestoplast 750	%	-	5.0%	-
Plasticizer	Napvis D-10	%	-	-	5.0%
Oil	Primol 352	%	19.0%	19.0%	-
Resin	MBG-278	%	35.0%	20.0%	-
Resin	Regalite (R)-R 91	%	-	20.0%	-
Resin	Escorez 5380	%	-	-	25.0
Antioxidant	Irganox 1010	%	1.0%	1.0%	0.4%

Table 1b):

Properties of the hotmelt adhesives

Property	Example 1	Example 2	Comparison
Melt viscosity [mPas] at 150°C	1485	1137	4580
Needle penetration [(100/25/5) 0.1 mm]	42	89	17
Softening point [°C]	79	76	96

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Table 1c):

Adhesion values of the film/nonwoven bonds

a) Adhesive sprayed onto film

Adhesion values	Example 1 A	Example 2 A	Comparison Example A	Example 1 B
Coating in g m <sup>-2</sup>	ca. 3.6	ca. 3.4	4.0	ca. 4.0
Adhesion value in N cm <sup>-1</sup>	0.54	0.48	0.28	0.68
Adhesion value in N cm <sup>-1</sup> after ageing	0.84	0.64	0.20	0.78
Wet strength N · cm <sup>-1</sup>	1.22	0.62	0.12	0.80

b) Adhesive sprayed onto nonwoven

Adhesion values	Example 1 A	Example 2 A	Comparison Example A	Example 1 B
Coating in g m <sup>-2</sup>	3.6	ca. 3.4	3.8	ca. 3.6
Adhesion value in N cm <sup>-1</sup>	0.70	0.52	0.30	0.70
Adhesion value in N cm <sup>-1</sup> after ageing	0.84	0.63	0.26	0.62
Wet strength N · cm <sup>-1</sup>	1.28	0.62	0.08	0.54